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Gael Pallares, Antoine Grimaldi, Matthieu George, Laurent Ponson, Matteo Ciccotti. Quantitative Analysis of Crack Closure Driven by Laplace Pressure in Silica Glass. *Journal of the American Ceramic Society*, 2011, 94, pp.2613-2618. 10.1111/j.1551-2916.2011.04471.x . hal-00656883

**HAL Id: hal-00656883**

**<https://hal.science/hal-00656883>**

Submitted on 5 Jan 2012

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# Quantitative analysis of crack closure driven by Laplace pressure in silica glass

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December 21, 2010

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Submitted to Journal of the American Ceramic Society

## Abstract

Crack tips in silica glass in moist atmosphere are filled with an equilibrium liquid condensation of a few hundred nanometers length. Not only does this local environment affect the chemistry of slow crack propagation by stress corrosion, but it also has an important mechanical effect due to its highly negative Laplace pressure. The present article presents an original technique for measuring the physical properties

of the liquid condensation in terms of the Laplace pressure and critical condensation distance. This is achieved by combining in-situ atomic force microscopy (AFM) measurements of the condensate length and optical determination of the crack closure threshold in a double cleavage drilled compression (DCDC) specimen.

## 1 Introduction

Crack tips in silicate glasses in moist atmosphere are invariably filled with a stable liquid phase, mainly composed by water, due to the phenomenon of capillary condensation. This is due on one hand to the extremely hydrophilic nature of glass surfaces, that are generally perfectly wet by water, and on the other hand to the elevated stiffness of glass that makes cracks very sharp, the crack opening remaining limited to less than a few nanometers up to a distance of hundreds of nanometers to few microns. Macroscopic failure properties of materials being essentially governed by mechanisms taking place in the vicinity of the crack tip, such a liquid condensate has a potential for playing an important role on the propagation of the crack, in spite of its submicronic extension. First, it affects the chemistry allowing for crack propagation at low velocity by determining the local environmental condition for the stress-corrosion reactions at the crack tip. But it can also have a mechanical effect due to the highly negative Laplace pressure in the condensate that acts on the crack walls and is responsible for the closure of the crack when the stresses become lower than some threshold.

Although the presence of capillary menisci in glass fractures have been previously argued [?, ?] for elevated relative humidity, proper characterization by in-situ AFM measurements has been only recently achieved [?, ?]. An original application of AFM phase imaging techniques has made it possible to measure the length  $L$  of the condensate as a function of the stress intensity factor (SIF)  $K$ , that controls the crack opening profile<sup>1</sup>. For silica glass the condensation was shown to be at equilibrium with an atmosphere of moist nitrogen and the critical condensation distance  $H_c$  was measured for several values of the relative humidity [?]. Silica glass is particularly suited to investigate the physico-chemical properties of the capillary condensate since the stress-corrosion reaction does not involve corrosion products nor ion

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<sup>1</sup>The symbol  $K$  will stand for the macroscopic mode I stress intensity factor. When making the difference between external and internal forces, this will be called  $K_{Ext}$ .

exchange phenomena.

When measuring the  $K - L$  curves by AFM phase imaging as in Grimaldi et al [?], the range of measurable values is insufficient for estimating the Laplace pressure. It was shown that neglecting the mechanical effect of the Laplace pressure on the crack opening profile induces a bias in the estimate of the critical distance  $H_c$  which was limited to within 15% [?]. The present work presents an important extension of the previous technique, which allows for the concomitant determination of both the critical condensation distance  $H_c$  and the Laplace pressure  $-\Delta P$  in the condensate<sup>2</sup>, and thus leads to a complete unbiased characterization of the physical properties of the wetting liquid.

## 2 Mechanical effect of capillary forces

When a hydrophilic solid is in equilibrium with a moist atmosphere, capillary condensation is expected to fill all gaps which are smaller than a critical distance  $H_c$ , that can be related to the Kelvin radius and to the wetting properties [?]. For a sharp crack with an opening profile  $f(X)$  this implies a condensation length  $L$  given by the condition (cf. Fig. ??):

$$f(X = L) = H_c \quad (1)$$

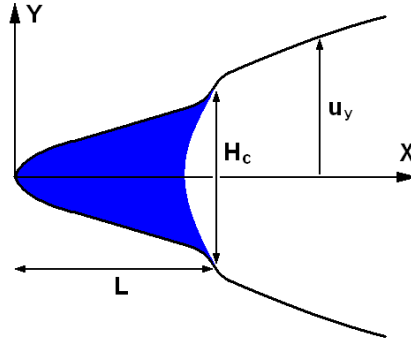


Figure 1: Schematic representation of an open crack showing how a capillary condensate modifies the crack opening profile near the crack tip.

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<sup>2</sup>The Laplace pressure  $-\Delta P$  ( $\Delta P > 0$ ) is the difference between the pressure of the condensed liquid phase and the moist atmosphere at equilibrium. The pressure in the condensate is assumed to be constant and independent of the crack profile geometry because its value is governed by the radius of curvature of the meniscus that is a function of relative humidity. In addition, the fluid is at rest in the condensate, insuring a homogeneous pressure.

When neglecting the effect of capillary forces, the crack opening profile can be modelled according to the Irwin solution<sup>3</sup>:

$$\delta = 2u_y(X, 0) = f(X) = \frac{2K}{E'} \sqrt{\frac{8X}{\pi}} \quad (2)$$

where  $E'$  is an effective elastic modulus<sup>4</sup>,  $X$  the distance from the crack tip and  $u_y(X, 0)$  the elastic displacement of the crack lips. Using relation (??) we obtain the following relation for equilibrium  $K - L$  curves:

$$L(K, H_c) = \frac{\pi}{8} \left( \frac{E' H_c}{2K} \right)^2 \quad (3)$$

that was used by Grimaldi et al [?] to estimate  $H_c$  without knowing the Laplace pressure. This relation has the form of an inverse square dependence of  $L$  on  $K$  and does not account for a closure threshold.

Capillary forces can be modelled as the action of a constant internal negative Laplace pressure  $-\Delta P$  between the crack lips when the crack opening is less than a distance  $H_c$ :

$$\sigma_{yy} = \begin{cases} -\Delta P & \delta \leq H_c \\ 0 & \delta > H_c \end{cases} \quad (4)$$

*i.e.* when the distance  $X$  from the crack tip is less than  $L$ . This internal force distribution is completely equivalent to the Dugdale formalism for the cohesive zone in ductile fracture [?], and thus presents the same solutions. The solutions for the crack opening profile can be written as the superposition of two terms respectively related to the external and internal forces<sup>5</sup>:

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<sup>3</sup>The Irwin solution is only valid in a close neighborhood of the crack tip, which is estimated to  $X < 15 \mu\text{m}$  in the Appendix for our sample geometry. This is comfortably satisfied since the observed condensate lengths are always smaller than  $4 \mu\text{m}$ .

<sup>4</sup> $E' = E/(1 - \nu^2)$  refers here to the plane strain Young's modulus. Indeed, we make such an assumption in our 2D model since most of the measurements such as the crack closure conditions will be measured in the mid plane of the sample, where such plane strain conditions prevails. The characterization of the condensate properties at the free surface of the sample will be justified in the discussion part.

<sup>5</sup>The procedure used here closely follows the approach described in Lawn (1993) p. 59 [?]. The problem is solved as the superposition of two solutions. The superscript 'Ext' refers to the solution where only the external forces are applied, *i.e.* the macroscopic forces applied to the sample grips, as in equation (??). The superscript 'Int' refers to the solution where only the internal forces are applied, *i.e.* the microscopic capillary forces acting between the crack lips. The superscript 'Tot' refers to the sum of these two solutions, which corresponds to the real problem. We should stress that the term  $K_{Tot}$

$$K_{Tot} = K_{Ext} + K_{Int} \quad u_y^{Tot} = u_y^{Ext} + u_y^{Int} \quad (5)$$

For small condensate length<sup>6</sup>, the contribution of the internal forces can be written as [?]:

$$K_{Int} = -\sqrt{\frac{2}{\pi}} \Delta P \int_0^L \frac{dX}{\sqrt{X}} = -\Delta P \sqrt{\frac{8L}{\pi}} \quad X, L \ll c \quad (6)$$

$$u_y^{Int}(X, 0) = \frac{K_{Int}}{E'} \sqrt{\frac{8X}{\pi}} - \frac{1}{2} \frac{K_{Int}}{E'} \sqrt{\frac{8L}{\pi}} \left[ \sqrt{\frac{X}{L}} - \frac{1}{2} \left( 1 - \frac{X}{L} \right) \ln \left| \frac{\sqrt{\frac{X}{L}} + 1}{\sqrt{\frac{X}{L}} - 1} \right| \right] \quad (7)$$

The new condensation length can be obtained by applying the condition (??) to these new solutions<sup>7</sup>.

The equilibrium  $K_{Ext} - L$  curve becomes:

$$2u_y(L) = \frac{2K_{Ext} + K_{Int}}{E'} \sqrt{\frac{8L}{\pi}} = H_c \quad (8)$$

This modelling predicts a crack closure threshold  $K_0$  when the condition  $K_{Tot} = K_{Ext} + K_{Int} = 0$  is satisfied, *i.e.*  $K_{Int} = -K_{Ext} = -K_0$ . By combining Eqs. (??) and (??), the threshold can be expressed as:

$$K_0 = \sqrt{E' H_c \Delta P} \quad (9)$$

This can be easily related to the adhesion energy [?]:

$$G_0 = w = \int_0^\infty \sigma_{yy} du_y = \int_0^{H_c} \Delta P du_y = \Delta P \cdot H_c \quad (10)$$

by using the equivalence  $G_0 = K_0^2/E'$ . At crack closure, the condensate length assumes a maximum value  $L_{max}$  given by:

$$L_{max} = \frac{\pi}{8} \frac{E' H_c}{\Delta P} = \frac{\pi}{8} \frac{K_0^2}{\Delta P^2} \quad (11)$$

Let us note that the leading term proportional to  $\sqrt{X}$  in the development of the crack profile vanishes at the onset of crack closure, so that the crack opening evolves as  $u_y(X) \simeq \frac{K_{Ext}}{E'} \frac{2}{\pi} \frac{X^{3/2}}{L}$  in the vicinity of

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corresponds to the loading felt by the silica at the crack tip.

<sup>6</sup>This corresponds to the small size yield approximation of the Dugdale model. The domain of validity of this approximation is  $L < 15 \mu\text{m}$  (cf. Appendix), which is also satisfied.

<sup>7</sup>The term in brackets in equation (??) can be easily verified to equal unity for  $X = L$ .

the tip ( $X \ll L$ ) for  $K_{Ext} = K_0$ . We remark that  $K_0$  and  $L_{max}$  naturally constitute two characteristic values for  $K$  and  $L$ , emerging from the values of  $E'$ ,  $H_c$  and  $\Delta P$ . The  $K_{Ext} - L$  curves (??) can thus be expressed in an elegant dimensionless form<sup>8</sup>:

$$\frac{L}{L_{max}} = \left( \frac{K_{Ext}}{K_0} - \sqrt{\left( \frac{K_{Ext}}{K_0} \right)^2 - 1} \right)^2 \quad (12)$$

In the limit of large loadings ( $K_{Ext} \gg K_0$ ), we recover from this formula the variations of  $L \propto 1/K_{Ext}^2$  found when the mechanical effect of the condensate is neglected (Eq. ??). As discussed previously, it is difficult to adjust both parameters by only using the  $K_{Ext} - L$  curves determined by AFM phase imaging. However, if the closure threshold  $K_0$  is measured independently, it is then easy to adjust the parameter  $L_{max}$  on the  $K_{Ext} - L$  curves. This allows to have an unbiased and robust measurement of both the critical condensation distance  $H_c$  and the Laplace pressure according to the inverse relations:

$$\Delta P = K_0 \sqrt{\frac{\pi}{8L_{max}}} \quad H_c = \frac{K_0}{E'} \sqrt{\frac{8L_{max}}{\pi}} \quad (13)$$

### 3 Experimental procedure and results

#### 3.1 In-situ monitoring of slow crack propagation

Fractures are initiated and propagated on a DCDC setup [?] at a constant temperature of  $(25.5 \pm 0.5)^\circ C$  in a leak-proof chamber under an atmosphere composed of air and water vapor at a given relative humidity level  $RH = (39 \pm 2)\%$ . The parallelepipedic DCDC samples ( $4 \times 4 \times 40 \text{ mm}^3$ , with  $10 \text{ }\mu\text{m}$  tolerance) of pure silica glass (Suprasil 311, Heraeus, Germany) were polished to a RMS roughness of  $0.25 \text{ nm}$  (for an area of  $10 \times 10 \text{ }\mu\text{m}^2$ ) and a hole of radius  $R = 0.5 \text{ mm}$  was drilled at their center to trigger the initiation of

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<sup>8</sup>Multiplying equation (??) by  $\Delta p$  we obtain:

$$\begin{aligned} E' H_c \Delta P &= (2K_{Ext} + K_{Int}) \Delta P \sqrt{\frac{8L}{\pi}} \\ K_0^2 &= (2K_{Ext} + K_{Int})(-K_{Int}) \\ K_{Int}^2 + 2K_{Int}K_{Ext} + K_0^2 &= 0 \\ K_{Int} &= -K_{Ext} + \sqrt{K_{Ext}^2 - K_0^2} = -\Delta P \sqrt{\frac{8L}{\pi}} \end{aligned}$$

and using equation (??) we easily obtain the dimensionless form (??).

two symmetric fractures of length  $c$  shown in Fig. ???. The hole's radius is evaluated precisely for each sample by optical microscopy.

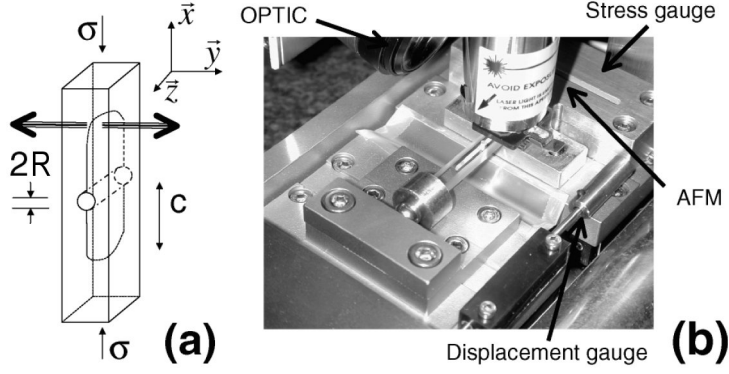


Figure 2: Experimental setup: (a) Sketch of the DCDC geometry; (b) picture of the experiment.

For an applied external compressive stress  $\sigma$ , the SIF  $K_{Ext}$  is determined as a function of the crack length according to the Eq. (??) in the Appendix. By coupling optical and atomic force microscopy (Nanoscope 3a, Veeco Metrology Inc, Santa Barbara, CA), the crack propagation velocity can be measured from  $10^{-5}$  m/s down to  $10^{-12}$  m/s. The details of the technique can be found in [?].

### 3.2 Measurement of condensate length by AFM phase imaging

AFM observations are done in tapping mode with AFM tips having a nominal radius of  $R_{tip} \sim 10$  nm (DNP, MPP-11100-10, Veeco Metrology Inc, Camarillo, CA). The tip is oscillated at constant frequency  $\omega$  (close to the resonance frequency  $\omega_0$ ). The oscillation amplitude  $A$  is kept constant to a set value thanks to a feedback loop controlling the vertical position of the scanner. The phase delay ( $\vartheta \in [-\pi : 0]$ ) between the stimulation and the oscillation of the tip can be related to the energy  $E_D$  dissipated per cycle by the tip-surface interactions [?]:

$$E_D = \frac{\pi k A^2}{Q} \left( -\frac{A}{A_0} \sin \vartheta - \frac{\omega}{\omega_0} \right) \quad (14)$$

where  $k$ ,  $Q$ ,  $A_0$  are respectively the stiffness of the AFM cantilever, the quality factor, and the free resonance amplitude. Fig. ?? shows typical height and phase images of the crack tip. The crack plane intersects perpendicularly the observed external surface of the sample. The region along the crack, characterized by a strong phase contrast, corresponds to the portion of the crack cavity which is filled by



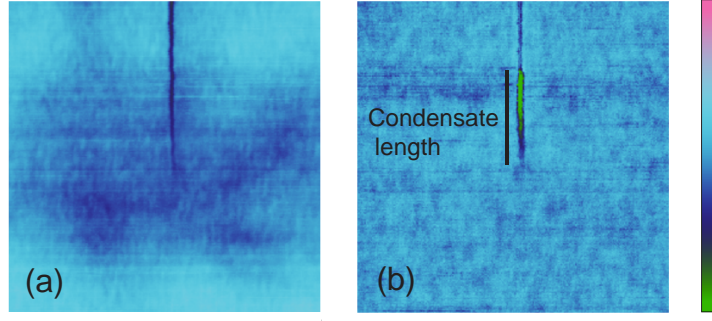


Figure 3: Typical AFM height (a) and phase (b) images of the crack tip for a fracture propagating from top to bottom of the image ( $400 \times 400 \text{ nm}^2$ ). The scale range is respectively 5 nm and  $5^\circ$ .

a condensed liquid phase. According to Eq. (??), the phase contrast on the condensate region corresponds to an increase in the energy dissipated by the tip-sample interaction [?]. Under humidity, the presence of thin water films on both the external sample surface and the AFM tip entails energy dissipation due to the combination of two phenomena: (1) the formation and rupture of a capillary bridge at each oscillation of the AFM tip [?] and (2) the visco-elastic displacement in the thin films [?]. The dissipated energy is very weak when scanning the glass surface, but it is greatly enhanced when the AFM tip crosses a portion of the crack tip filled with liquid water [?]. The resolution of the AFM technique does not allow to measure the opening of the crack accurately (a few nanometers here), but it allows to measure the length  $L$  of the condensed region, ranging between 100 nm and 400 nm in our experiments, with an incertitude lower than 10 nm. Each estimate of the condensate length  $L$  is the average of three measurements on images with an optimized scan size. The measurement was shown not to be dependent on the AFM working conditions, nor on the details of the AFM tip shape and its chemical nature within the given incertitude. The weak crack propagation velocity during the test was previously shown not to affect the equilibrium length of the condensate [?]. In order to avoid aging phenomena and to provide an optimum mode I loading condition, it is preferable to make each determination of the  $K_{Ext} - L$  curve on a new specimen just after the crack initiation. The results are reported in Fig. ?? for five different samples and we remark an excellent reproducibility.

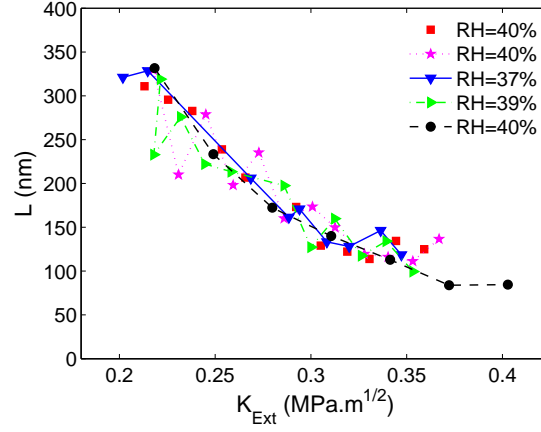


Figure 4: Condensate length  $L$  as a function of the stress intensity factor  $K_{Ext}$  obtained by AFM.

### 3.3 Measurement of crack closure threshold by optical microscopy

It is well known that when the external stresses are reduced below some threshold, cracks in glass are observed to progressively close [?, ?]. In order to perform the measurement of the crack closure by using the same loading setup and the same environmental conditions as for the  $K_{Ext} - L$  curves, we can use the optical microscope associated to the AFM system. When measuring  $K_{Ext} - L$  curves, the crack front is vertical in order to image the crack tip by AFM at the free surface of the sample (cf. Fig. ??). In order to observe the crack closure, the DCDC sample is rotated by  $90^\circ$ , the fracture front laying horizontally according to Fig. ?. The white light source illuminates the sample vertically, after passing through the optical axis of the CCD camera and after being reflected by an inclined mirror in the AFM head. The field of view of the camera is  $920 \mu\text{m}$  and the resolution is limited by the pixel size to  $10 \mu\text{m}$ .

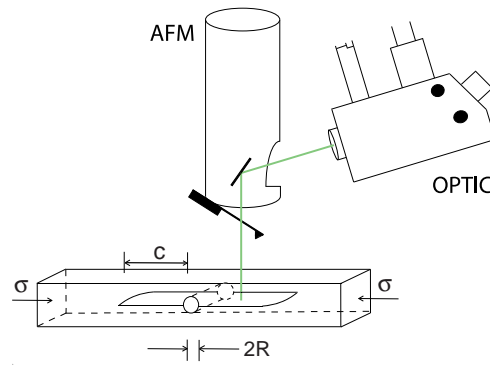


Figure 5: Sketch of the DCDC sample arranged to observe the crack closure by optical microscopy (horizontal crack plane)

For the same reasons discussed for  $K_{Ext} - L$  curves, it is again preferable to make each determination of the closure threshold on a new specimen just after the crack initiation. The new crack is propagated for a convenient crack length ( $c > w = 2$  mm) until the propagation velocity becomes less than  $10^{-9}$  m/s, in order to avoid any further optically observable propagation during the measurement. Then, we continuously decrease the stress to a rate of 0.12 MPa/s and monitor the evolution of the crack front position, and thus the crack length, with an acquisition frequency of 1 image/second as reported in Fig. ??.

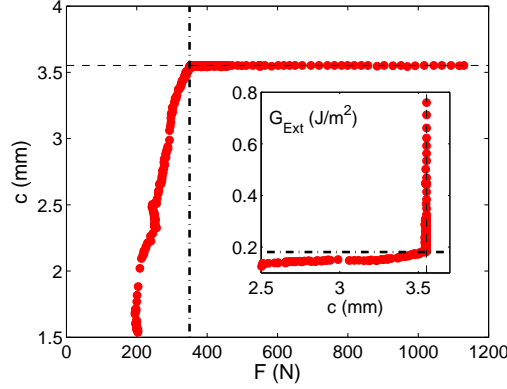


Figure 6: Evolution of the apparent crack length  $c$  as a function of the external decreasing load  $F$ . In the inset the same data are plotted in terms of the strain energy release rate  $G_{Ext} = K_{Ext}^2/E'$  as a function of the apparent crack length  $c$  (NB: the axes are switched because  $c$  should now be considered as the independent variable). The crack closure threshold  $G_0$  corresponds to the intersection between the two regimes.

According to the modelling proposed in section ??, the crack opening profile undergoes two regimes: in a first stage of the unloading the crack length will remain constant, while the crack opening profile is progressively reducing and the condensate length is increasing. When the external SIF reaches the threshold value  $K_0$ , the contribution of internal and external forces is perfectly balanced, the crack tip singularity vanishes and the condensate length assumes the maximum value  $L_{max}$ . By further decreasing the external load the system enters another regime where the crack closes progressively. The threshold value  $K_0$  is then accurately determined by measuring the load and the crack length<sup>9</sup> at the transition

<sup>9</sup>The exact position of the crack tip can not be perceived optically since the reflectivity of the glass-water interface is very weak, but  $L_{max}$  will be shown to be of the order of  $4 \mu\text{m}$ , which is smaller than the optical resolution.

point (Fig. ??). The average over three tests in moist atmosphere with  $RH = (40 \pm 3)\%$  is:

$$K_0 = (0.114 \pm 0.006) \text{ MPa.m}^{1/2} \quad G_0 = (180 \pm 20) \text{ mJ/m}^2$$

where we used the elastic moduli of silica glass<sup>10</sup>  $E = (72 \pm 2) \text{ GPa}$  and  $\nu = (0.170 \pm 0.005)$ .

### 3.4 Estimate of the Laplace pressure

Although none of the previous techniques allows the complete solution of the problem, their combination does. Indeed, we can insert the measured value of  $K_0 = (0.114 \pm 0.006) \text{ MPa.m}^{1/2}$  into equation (??) and adjust the single missing parameter  $L_{max}$  on the  $K_{Ext} - L$  curves. The fit is well conditioned and the result is shown in Fig. ?. We find:

$$L_{max} = (4 \pm 1) \text{ }\mu\text{m}$$

By using equations (??) we determine the values of the critical distance  $H_c$  and of the Laplace pressure  $\Delta P$ :

$$H_c = (5.0 \pm 0.7) \text{ nm} \quad \Delta P = (36 \pm 5) \text{ MPa}$$

## 4 Discussion and Conclusion

Although several measurements exist in the literature for the closure threshold in glass [?, ?, ?, ?], it is the first time that they are combined with an in-situ observation of the length of a liquid condensate. This allows us providing both a sound physical interpretation of the crack closure phenomenon and a complete characterization of the physical parameters of the wetting liquid in terms of its Laplace pressure and critical condensation distance.

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<sup>10</sup>Silica glass is known to exhibit non-linear elastic deformation according to [?]:

$$\frac{\Delta E}{E} = (1 + 5.75\epsilon)$$

However, in the present analysis the crack tip stresses are limited by the Laplace pressure  $\Delta P \sim 40 \text{ GPa}$  ( $\epsilon \sim 0.05\%$ ). The maximum effect on the elastic modulus is thus of the order of 0.3%, which is negligible for our purposes.

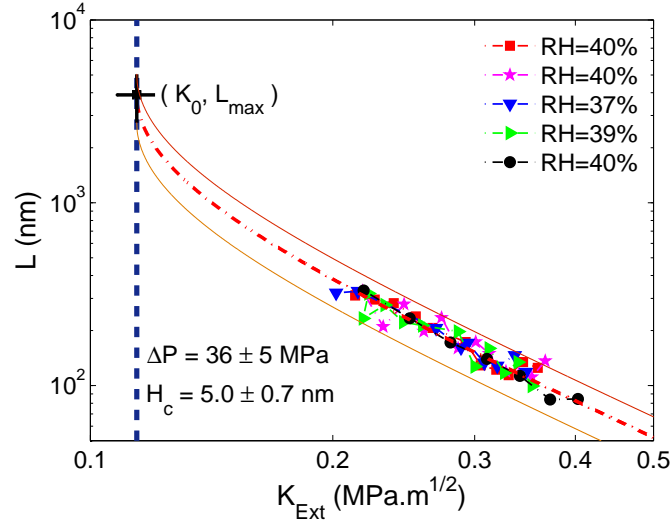


Figure 7: Fit of the  $K_{Ext} - L$  curve according to equation (??). The AFM measurements of Fig. ?? are combined with the optical measurements of the threshold  $K_0$  (vertical dashed line). The black square symbol corresponds to the estimated value of  $L_{max}$ .

The value of the adhesion energy  $G_0 = (180 \pm 20) \text{ mJ/m}^2$  is in good agreement with other determinations in the literature ranging between 100 and 200  $\text{mJ/m}^2$  (*ibid.*), which are generally roughly compared to the energy required to create two water surfaces ( $2\gamma_w \sim 144 \text{ mJ/m}^2$ ). According to more sophisticated modeling [?], the adhesion energy in perfect wetting conditions is expected to exceed the surface tension term.

Our simple modelling accounts for the crack closure by the action of capillary forces and it neglects other kinds of interactions between the solid surfaces. This is also in agreement with the observed independence of the closure threshold on the glass nature [?], and with similar conjectures formulated by Rayleigh [?] and Lawn *et al.* [?]. Several other interpretations of the crack closure have been proposed ranging from hydrogen bond interaction between adsorbed water molecules to alkali ion bridging or partial reformation of  $SiOSi$  bonds between opposite crack surfaces [?]. However, they result from observations of the crack closure behavior on alkali containing glasses after several aging or thermal treatments. The present study avoids all ambiguity since it is performed on freshly fractured silica glass samples in very clean conditions. Although the cracks were produced by stress-corrosion, no corrosion products are expected at ambient conditions in silica since the silanol groups remain bonded to the crack walls and our  $K_{Ext} - L$  measurements were stable on several days periods. In a previous paper [?], we reported

larger values for the condensate length and critical distance, but these were taken on a sample that had been aged for one year in primary vacuum. A detailed study of the aging behavior is out of the scope of the present work and will be published later.

It is the first time that the Laplace pressure is measured for a capillary condensation inside a crack tip. We remark that the reported value  $\Delta P = (36 \pm 5)$  MPa corresponds to a very negative pressure inside the liquid phase and the remarks given above suggest that this condensed phase is very close to pure water. The stability of this phase is provided by the high degree of confinement which prevents nucleation of vapor bubbles [?]. Although the largest reported measured negative pressures are around -140 MPa [?], the most reliable ones are around -20 MPa [?]. By combining this technique with a low humidity environmental chamber, it will be possible to obtain important data on the behavior of water at very negative pressure [?, ?].

An important remark concerns the opportunity of comparing  $K_{Ext} - L$  curves that are measured at the sample surface with threshold measurements performed by observing the crack front in the bulk of the sample. Our modelling of the mechanical behavior of the DCDC sample, and in particular, the determination of the value of SIF, has been performed by a two dimensional plane strain analysis, which describes accurately the behavior in the bulk of the specimen. However, the recent application of digital image correlation techniques to the measurement of the surface displacement fields near the crack tip in our DCDC specimens have shown an excellent agreement between the values of the stress intensity factor determined at the surface and the values determined by a macroscopic determination according to two dimensional models of the DCDC sample [?].

Incidentally, we remarked a significant hysteresis between the closure and reopening behavior of the crack as previously observed in Refs. [?, ?, ?]. Moreover, while our equilibrium modelling would predict a constant stress intensity factor during the progression of the crack closure, a decrease of the threshold is observed during the closure at constant load rate (cf. Fig. ??), followed by a progressive increase when the loading process is arrested. These observations suggest the presence of irreversible processes that are not simply related to a velocity dependence as suggested in [?]. For that reasons, we limited our determinations of the threshold to the onset of the first closure, while leaving these interesting observations to future investigations.

The present results cast a clearer light on the physical mechanisms of crack closure in glasses, which

are intimately related to capillary forces. The elevated stiffness of these materials along with the high degree of chemical inertness of silica glass have allowed original and reproducible measurements of the condensate length. This precious ingredient, combined with the measurement of the adhesion energy through the crack closure threshold, allows obtaining an estimate of the Laplace pressure, and thus a complete characterization of the physical properties of the condensed phase.

## Acknowledgement

We thank E. Charlaix, M. Flemming and T. Fett for fruitful discussion. This work was supported by the ANR Grant “Corcosil” No. ANR-07-BLAN-0261-02. L. Ponson is supported by the European Union through the “Phycracks” Marie Curie fellowship.

## Appendix: 2D modelling of the DCDC specimen and small condensate approximation

For a DCDC specimen of dimensions  $2w \times 2t \times 2\ell$ , containing a hole of radius  $R$  and two symmetric cracks of length  $c$  (cf. Fig. ??), the stress intensity factor  $K_{Ext}$  caused by the external loading  $\sigma = F/4wt$  can be accurately approximated by the following dimensionless expansion in terms of the ratios  $c/R$  and  $w/R$  [?]:

$$\frac{\sigma\sqrt{\pi R}}{K_{Ext}} = \left[ C_0 + C_1 \frac{w}{R} + C_2 \left( \frac{w}{R} \right)^2 \right] + \left[ C_3 + C_4 \frac{w}{R} + C_5 \left( \frac{w}{R} \right)^2 \right] \frac{c}{R} \quad (15)$$

with the set of parameters:  $C_0 = 0.3156$ ,  $C_1 = 0.7350$ ,  $C_2 = 0.0346$ ,  $C_3 = -0.4093$ ,  $C_4 = 0.3794$ , and  $C_5 = -0.0257$  for  $2.5 \leq w/R \leq 5$  and  $w < c < \ell - 2w$ . For our geometry, this reduces to:

$$\frac{\sigma\sqrt{\pi R}}{K_{Ext}} = 3.547 + 0.650 \frac{c}{R} \quad (16)$$

In the absence of internal forces, the crack opening profile was shown [?] to be described by a fifth order Williams expansion [?] with 1% accuracy when  $X < 0.85w = 1.7$  mm:

$$u_y(X) = \frac{K_I}{E'} \sqrt{\frac{8}{\pi}} \sqrt{X} \left( 1 + 1.319 \left( \frac{X}{w} \right) + 0.515 \left( \frac{X}{w} \right)^2 \right). \quad (17)$$

This expression remains valid as far as the effects of the finite size of the specimen are not relevant, *i.e.* for  $2.5w - R < c < L - 2.3w - R$ . The range of 1% validity of the first order term, corresponding to the Irwin equation (??) used in the present work, is thus  $X < 0.0076w = 15 \mu\text{m}$  [?].

The stress intensity factor caused by a generic distribution of internal forces along the crack faces can be calculated according to the weight function procedure developed by Bueckner [?]:

$$K_{Int} = \int_0^c h(c, X) \sigma_{yy}(X) dX \quad (18)$$

where the weight function  $h(c, X)$  does not depend on the stress distribution, but only on the geometry of the specimen. The mode I weight function for the DCDC geometry were approximated by Fett et al. [?] by finite element simulation, and can be rewritten according to our formalism:

$$h_I(c, X) = \sqrt{\frac{2}{\pi X}} \left( 1 + D_1^{(I)} \frac{X}{c} + D_2^{(I)} \left( \frac{X}{c} \right)^2 \right) \quad (19)$$

where  $D_1^I$  and  $D_2^I$  were fitted by the following development in the range  $0 \leq c/R \leq 8$ :

$$\begin{aligned} D_1^{(I)} &= -3.97 + 1.466 \frac{c}{R} + 4.533 \exp \left( -0.291 \frac{c}{R} \right) \\ D_2^{(I)} &= -0.246 + 0.222 \frac{c}{R} + 0.529 \exp \left( -2.08 \frac{c}{R} \right) \end{aligned} \quad (20)$$

In our measurements the crack length ranges between 3 and 5 mm, corresponding to  $c/R$  ranging between 5.66 and 9.43. Although the upper end is slightly higher than the domain where the former development were adjusted, the behavior of the equations (??) is quite linear near  $c/R = 8$ . It is thus sound to extrapolate for estimate purpose the values  $D_1^{(I)} = 10.152$  and  $D_2^{(I)} = 1.848$  that correspond to the largest corrections. The range of 1% validity of the small condensate approximation, corresponding to the first term of equation (??) is thus  $X < 15 \mu\text{m}$  for our DCDC geometry. Since this domain of validity is always larger than the condensate length, this justifies the use of a global first order approximation in all our modelling.



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